

(บริษัท พรีเมียม จำกัด (มหาชน))

(งานโครงสร้าง)

โครงการ : VEHHA HUA HIN

Project Alliance Co., Ltd.

By: TB

Date: 09-04-67

23 เมษายน 2567

วันที่ 9 เมษายน 2567

กำหนดตอบกลับวันที่

เอกสารขออนุมัติทั่วไป

1. เรื่อง : ขอนำส่ง แบบพื้น Post-tensioned slab ชั้น 19 พร้อมรายการคำนวณ
 ถึง : บริษัท โปรเจ็ค แอลโลเอ็นซ์ จำกัด
 เรียน : คุณวุฒิเลิศ ทองดี
 ผู้จัดการ - โครงการ
 เอกสารแนบ : แบบพื้น Post-tensioned slab ชั้น 19 พร้อมรายการคำนวณ จำนวน 1 ชุด
 รายละเอียด : ☒ เพื่อพิจารณา ☐ อื่นๆ
 พร้อมแนบค่าแรงของชั้น 19 มาด้วย พร้อมลายเซ็นรับรองของทีม VE และได้ให้ทางผู้ออกแบบตรวจสอบและชี้แจงรายการคำนวณ-
 ปริมาณลวด ตาม Attachment-1 ข้อ 1, 2 และ 4 แล้ว ตามเอกสารแนบทั้งหมด

ลงนาม (ว่าที่ ร.อ.สัญญาลักษณ์ ปรีชา)
 วันที่ 9 / 04 / 67 ผู้จัดการโครงการ

2. ถึง : บริษัท อาริเทคเซอแรล เอ็นจิเนียริง 49 จำกัด
 เรียน : คุณอรรถพัทธ์ อวัญ
 รายละเอียด : ☒ เพื่อพิจารณา ☐ อื่นๆ
 บันทึก : ขอส่งรายการคำนวณและแบบโครงสร้างพื้น Post-Tension ชั้น 19 เพื่อให้ผู้ออกแบบพิจารณาตรวจสอบและอนุมัติต่อไปครับ
 PAC ได้ตรวจสอบและ Cloud ในจุดที่แตกต่างกัน และจำนวน Tendon ในแบบ For Construction และแบบ VE (ตามเอกสารแนบ)
 ลงนาม (คุณวุฒิเลิศ ทองดี)
 วันที่ 11 / 04 / 67 ผู้จัดการโครงการ
 เวทีศ หงษ์พนัส

3. ถึง : บริษัท โปรเจ็ค แอลโลเอ็นซ์ จำกัด
 เรียน : คุณวุฒิเลิศ ทองดี
 รายละเอียด : ☐ ไม่ขัดข้อง ☒ ไม่ขัดข้องแต่มีความคิดเห็นเพิ่มเติม ☐ ให้จัดส่งใหม่
 บันทึก : SEE ATTACHMENT-1
 ลงนาม (อรรถพัทธ์ อวัญ)
 วันที่ 10 / 05 / 24

4. ถึง : บริษัท พรีเมียม จำกัด (มหาชน)
 เรียน : ว่าที่ ร.อ.สัญญาลักษณ์ ปรีชา
 รายละเอียด : ☐ ไม่ขัดข้อง ☒ ไม่ขัดข้องแต่มีความคิดเห็นเพิ่มเติม ☐ ให้จัดส่งใหม่
 บันทึก : ให้ดำเนินการตามคำตอบของผู้ออกแบบ
 ลงนาม (คุณวุฒิเลิศ ทองดี)
 วันที่ 10 / 05 / 67 ผู้จัดการ-โครงการ
 เวทีศ หงษ์พนัส

5. สำเนาถึง : ☐ ผู้รับเหมาอื่นๆ ☒ ผู้ออกแบบ AE49 ☒ เจ้าของโครงการ HSL

1. เนื่องจากการปรับ Concept การออกแบบโดยใช้วิธี Nonlinear และเปลี่ยนโครงสร้างเสาเดิมเป็นระบบกำแพงรับแรงเฉือนที่ทีม VE ได้เปลี่ยนแปลงมา แรงในพื้นที่ทั้งแรงดัดและแรงเฉือนจึงต้องมีการเปลี่ยนแปลงไปจากเดิม ดังนั้นจึงอนุมัติบนเงื่อนไขว่ารายการคำนวณและแบบที่ส่งมาได้มีการเปลี่ยนแปลงและใช้แรงดัดและแรงเฉือนตาม Concept Design ใหม่ของทีม VE ทุก Span อย่างถูกต้องเนื่องจากไม่มีรายการคำนวณครบทุกแฉกแฉกที่แตกต่างกัน

1. กรุณาส่งล่วงหน้าไม่น้อยกว่า 10 วันทำการเนื่องจากเป็นรายการที่ต้องใช้เวลาในการตรวจสอบมาก ในกรณีที่จำเป็นต้องแก้ไข อาจทำให้มีผลกับระยะเวลาการก่อสร้าง
2. นับแต่ชั้น 9 เป็นต้นไป ขอให้ทางทีม VE ลงลายมือชื่อในการตรวจสอบรายการคำนวณร่วมกับผู้ออกแบบ เนื่องจากเป็นผู้ร่วมคำนวณออกแบบและเป็นผู้ให้ค่าแรงดัดและแรงเฉือนในการวิเคราะห์แรงในระบบพื้น Post Tensionก่อนส่งมาให้ AE49 อนุมัติ เพื่อความถูกต้องของข้อมูลต่อไป

ATTACHMENT 1 (1/1)

COLUMN STRIP	Wind			EarthQuake		
	MX	MY	V	M2	M3	V
C6	-14.99	-8.79	8.40	-4.37	-2.85	2.85
C7	-15.59	-18.85	6.24	-3.94	-6.93	6.93
C8	-28.36	-21.77	13.12	-5.92	-7.62	7.62
C9	-19.57	-23.65	7.83	-3.24	-7.57	7.57
C10_Grid8	-12.76	0.00	7.74	-2.12	0.00	1.32
C10_Grid9	-27.86	-40.46	14.41	-5.08	-13.99	13.99
C10_Grid10	-37.06	-40.19	17.66	-7.21	-12.17	12.17
C11	-46.29	-41.72	23.28	-10.09	-11.57	11.57
C12	-26.24	-30.87	25.63	-6.72	-10.77	10.77
C13	-16.31	-21.92	13.71	-4.42	-6.88	6.88
C17	-6.34	-9.66	12.05	-2.76	-4.36	5.68
C18	-3.33	-1.52	4.01	-1.00	-0.61	1.65
C19	-0.57	-1.84	2.07	-0.19	-0.51	0.51
C20	-0.65	-7.76	5.54	-0.16	-1.87	1.87
W1_L	0.00	-0.33	0.13	0.00	0.09	0.09
W2	-1.15	-29.03	7.67	-0.42	-10.53	10.53
W3	-36.28	-15.78	13.77	-8.53	-3.86	4.42

Grid B (ZONE 1)

C6 C7 C8 C9
 14.99 15.59 28.36 19.15
 ^ ^
 7.8 7.8 11.8 14.18

Grid C

C17 C18 C19 C20
 6.34 3.33 0.57 0.65

Grid B (ZONE 2)

C10 C10 C10 C11 C12 C13
 12.76 27.86 37.06 46.29 26.24 16.31
 ^ ^ ^ ^ ^
 13.93 13.93 24.71 12.35 21.04 25.25 8.27 18.13

รายการคำนวณ
POST – TENSIONED SLAB

โครงการ

VEHHA HUAHIN

19th FLOOR



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ADAPT-PT FOR POST-TENSIONED BEAM/SLAB DESIGN
Version 7.00 AMERICAN (ACI 318-99/UBC-77)
ADAPT CORPORATION - Structural Concrete Software System
1733 Woodside Road, Suite 220, Redwood City, California 94061
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PROJECT FILE: 19TH-B(Z-2)

PROJECT TITLE:
VEHHA HUAHIN
19TH-B(Z-2)

2 - INPUT GEOMETRY

2.1.1 PRINCIPAL SPAN DATA OF UNIFORM SPANS

S	T	F	LENGTH	WIDTH	DEPTH	TOP FLANGE width thick.	BOTTOM/MIDDLE FLANGE width thick.	REF HEIGHT	MULTIPLIER left	MULTIPLIER right
P	Y	O								
A	P	R								
N	E	M								
1	2	3	4	5	6	7	8	9	10	11
1	U	1	5.70	710.00	30.00					30.00
2	U	1	5.70	710.00	30.00					30.00
3	U	1	11.40	710.00	30.00					30.00
4	U	1	9.50	710.00	30.00					30.00
5	U	1	4.25	710.00	30.00					30.00

LEGEND:

1 - SPAN
C = Cantilever
2 - TYPE
U = Uniform; prismatic
N = Nonuniform section

3 - FORM
1 = Rectangular section
2 = T or I inverted section
3 = I section
4 = Expanded T or L section
7 = Joint
8 = Waffle
11 - Top surface reference line

2.2 - SUPPORT WIDTH AND COLUMN DATA

JOINT	SUPPORT WIDTH	LENGTH	LOWER COLUMN (DIA) D	CBC*	LENGTH	UPPER COLUMN B(DIA) D	CBC*
1	2	3	4	5	6	7	8
1	.00	3.25	35.00	(1)	3.25	400.00	35.00 (1)
2	.00	3.25	35.00	(1)	3.25	400.00	35.00 (1)
3	.00	3.25	400.00	35.00 (1)	3.25	400.00	35.00 (1)
4	.00	3.25	400.00	35.00 (1)	3.25	400.00	35.00 (1)
5	.00	3.25	400.00	35.00 (1)	3.25	400.00	35.00 (1)
6	.00	3.25	30.00	(1)	3.25	200.00	30.00 (1)

*THE COLUMN BOUNDARY CONDITION CODES (CBC)

Fixed at both ends ... (STANDARD) = 1
Hinged at near end, fixed at far end = 2
Fixed at near end, hinged at far end = 3
Fixed at near end, roller with rotational fixity at far end .. = 4

3 - INPUT APPLIED LOADING

<---CLASS---> <-----TYPE----->
D = DEAD LOAD U = UNIFORM P = PARTIAL UNIFORM
L = LIVE LOAD C = CONCENTRATED M = APPLIED MOMENT
Li = LINE LOAD

SW= SELF WEIGHT Computed from geometry input and treated as dead loading
Unit selfweight w = 2400.0 Kg/m³

SPAN	CLASS	TYPE	Intensity T/m ²	(From ... To) (m)	(M or C ... At) (T-m or T ... m)	Total on Trib T/m		
-1	2	3	4	5	6	7	8	9

1	L	U	.200	.00	5.70	1.420
1	D	U	.400	.00	5.70	2.840
1	D	Li		.00	5.70	.400
1	SW	U		.00	5.70	5.112
2	L	U	.200	.00	5.70	1.420
2	D	U	.400	.00	5.70	2.840
2	D	Li		.00	5.70	.400
2	SW	U		.00	5.70	5.112
3	L	U	.200	.00	11.40	1.420
3	D	U	.400	.00	11.40	2.840
3	D	Li		.00	11.40	.400
3	SW	U		.00	11.40	5.112
4	L	U	.200	.00	9.50	1.420
4	D	U	.400	.00	9.50	2.840
4	D	Li		.00	9.50	.400
4	SW	U		.00	9.50	5.112
5	L	U	.200	.00	4.25	1.420
5	D	U	.400	.00	4.25	2.840
5	D	Li		.00	4.23	.400
5	SW	U		.00	4.25	5.112

3.1 - LOADING AS APPEARS IN USER'S INPUT SCREEN PRIOR TO PROCESSING

SPAN	CLASS	TYPE	UNIFORM (T/m^2), LINE (T/m)	(CON. or PART.) (T@m or m-m)	(M O M E N T) (T-m @ m)
-1	-2	-3	-4	-5	-6
-7	-8				
1	L	U	.200		
1	D	U	.400		
1	D	L	.400	.00	5.70
2	L	U	.200		
2	D	U	.400		
2	D	L	.400	.00	5.70
3	L	U	.200		
3	D	U	.400		
3	D	L	.400	.00	11.40
4	L	U	.200		
4	D	U	.400		
4	D	L	.400	.00	9.50
5	L	U	.200		
5	D	U	.400		
5	D	L	.400	.00	4.25

NOTE: SELFWEIGHT INCLUSION REQUIRED

5 - DEAD LOAD MOMENTS, SHEARS & REACTIONS

SPAN	< 5.1 SPAN M(1)*	M O M E N T S Midspan	(Tm) M(r)*	< 5.2 SPAN SHEARS (T) > SH(1)	SH(r)
-1	-2	-3	-4	-5	-6
1	-18.12	12.58	-24.56	-22.67	24.93
2	-16.98	5.30	-40.26	-19.72	27.89
3	-85.91	46.24	-92.98	-46.99	48.23
4	-72.29	30.00	-56.15	-41.37	37.97
5	-30.09	3.19	-1.24	-24.54	10.95

Note:

* = Centerline moments

JOINT	< 5.3 REACTIONS (T) >	<- 5.4 COLUMN MOMENTS (Tm) ->
-1	-2	-3
-4	-5	-6
1	22.67	-9.43
2	44.65	3.95
3	74.87	-23.77
4	89.60	10.77
5	62.51	13.57
6	10.95	.65

6 - LIVE LOAD MOMENTS, SHEARS & REACTIONS

<-- 6.1 LIVE LOAD SPAN MOMENTS (Tm) and SHEAR FORCES (T) -->

SPAN	<---- left* ---->		<--- midspan --->		<---- right* ---->		<--SHEAR FORCE-->	
	max	min	max	min	max	min	left	right
-1	2	3	4	5	6	7	8	9
1	-3.08	-3.08	2.14	2.14	-4.18	-4.18	-3.85	4.24
2	-2.89	-2.89	.90	.90	-6.85	-6.85	-3.35	4.74
3	-14.61	-14.61	7.86	7.86	-15.81	-15.81	-7.99	8.20
4	-12.29	-12.29	5.10	5.10	-9.55	-9.55	-7.03	6.46
5	-5.12	-5.12	.54	.54	-.21	-.21	-4.17	1.86

Note:

* = Centerline moments

<- 6.2 REACTIONS (T) -> <----- 6.3 COLUMN MOMENTS (Tm) ----->

JOINT	<--- LOWER COLUMN --->		<--- UPPER COLUMN --->	
	max	min	max	min
-1	2	3	4	5
1	3.85	.00	.00	-1.60
2	7.59	.00	.67	.00
3	12.73	.00	.00	-4.04
4	15.23	.00	1.83	.00
5	10.63	.00	2.31	.00
6	1.86	.00	.11	.00

Note: Block 6.1 through 6.3 values are maxima of all skipped loading cases

8 - SUM OF DEAD AND LIVE MOMENTS (Tm)

Maxima of dead load and live load span moments combined
for serviceability checks (1.00DL + 1.00LL)

SPAN	<---- left* ---->		<--- midspan --->		<---- right* ---->	
	max	min	max	min	max	min
-1	2	3	4	5	6	7
1	-21.20	-21.20	14.72	14.72	-28.74	-28.74
2	-19.87	-19.87	6.20	6.20	-47.11	-47.11
3	-100.52	-100.52	54.10	54.10	-108.79	-108.79
4	-84.58	-84.58	35.10	35.10	-65.70	-65.70
5	-35.21	-35.21	3.73	3.73	-1.46	-1.46

Note:

* = Centerline

8 - SUM OF DEAD AND LIVE MOMENTS (Tm)

Maxima of dead load and live load span moments combined
for serviceability checks (1.00DL + 1.00LL)

SPAN	<---- left* ---->		<--- midspan --->		<---- right* ---->	
	max	min	max	min	max	min
-1	2	3	4	5	6	7
1	-21.20	-21.20	14.72	14.72	-28.74	-28.74
2	-19.87	-19.87	6.20	6.20	-47.11	-47.11
3	-100.52	-100.52	54.10	54.10	-108.79	-108.79
4	-84.58	-84.58	35.10	35.10	-65.70	-65.70
5	-35.21	-35.21	3.73	3.73	-1.46	-1.46

Note:

* = Centerline

9 - SELECTED POST-TENSIONING FORCES AND TENDON PROFILES

9.1 PROFILE TYPES AND PARAMETERS

LEGEND:

For Span:

- 1 = reversed parabola
- 2 = simple parabola with straight portion over support
- 3 = harped tendon

For Cantilever:

- 1 = simple parabola
- 2 = partial parabola
- 3 = harped tendon

9.2	TENDON		PROFILE		
	TYPE	X1/L	X2/L	X3/L	A/L
1	1	.100	.500	.100	.000
2	1	.100	.500	.100	.000
3	1	.100	.500	.100	.000
4	1	.100	.500	.100	.000
5	1	.100	.500	.100	.000

9.3 - SELECTED POST-TENSIONING FORCES AND TENDON DRAPE

Tendon editing mode selected: TENDON SELECTION

SPAN	FORCE (T/-)	SELECTED VALUES -< DISTANCE OF CGS (cm) ->			CALCULATED VALUES		
		Left	Center	Right	P/A (Kg/cm ²)	wbal (T/-)	wbal (%DL)
1	235.392	15.00	9.20	23.70	11.05	5.883	70
2	248.951	23.70	14.20	24.70	11.69	6.130	73
3	376.838	24.70	4.20	23.70	17.69	4.639	56
4	251.112	23.70	4.20	23.70	11.79	4.341	52
5	229.640	23.70	13.20	15.00	10.78	6.255	75

Approximate weight of strand 768.9 Kg

9.35 - TENDON SELECTION DATA:

TYPE	SEL.	FORCE (T)	TENDON EXTENTS				
			<1>	<2>	<3>	<4>	<5>
-1	2	3	4	5	6	7	8
A	21	11.30					
B	13	11.83					

9.5 REQUIRED MINIMUM POST-TENSIONING FORCES (T)

SPAN	BASED ON STRESS CONDITIONS ->			BASED ON MINIMUM P/A ->		
	LEFT*	CENTER	RIGHT*	LEFT	CENTER	RIGHT
1	.00	.00	.00	202.35	202.35	202.35
2	.00	.00	.00	202.35	202.35	202.35
3	.00	183.51	.00	202.35	202.35	202.35
4	.00	36.87	.00	202.35	202.35	202.35
5	.00	.00	.00	202.35	202.35	202.35

Note:
* = Centerline9.6 SERVICE STRESSSES (kg/cm²)(tension shown positive)

SPAN	LEFT*		CENTER		RIGHT*	
	TOP	BOTTOM	TOP	BOTTOM	TOP	BOTTOM
1	-8.66	-12.53	-15.35	-6.76	-9.70	-13.45
2	-11.02	-12.52	-9.14	-14.23	-14.49	-21.09
3	-7.79	-27.90	-40.28	4.90	-7.12	-29.49
4	-10.15	-26.41	-25.79	2.22	-4.97	-17.99
5	-8.61	-14.30	-9.73	-11.84	-10.35	-10.68

Note:
* = Centerline

9.7 POST-TENSIONING BALANCED MOMENTS, SHEARS & REACTIONS

SPAN	SPAN MOMENTS (Tm) -->			SPAN SHEARS (T) -->	
	left*	midspan	right*	SH(l)	SH(r)
1	10.39	-10.15	18.28	2.41	2.41
2	15.69	-8.91	28.69	.33	.33
3	44.35	-30.04	46.31	-.50	-.50
4	39.16	-20.18	29.34	-.12	-.12
5	19.29	-4.86	1.11	-.86	-.86

Note:
* = Centerline

<-- REACTIONS (T) -->

<-- COLUMN MOMENTS (Tm) -->

-joint-----	2-----	Lower columns-----	Upper columns-----
1	-2.414	5.409	4.979
2	2.082	-1.353	-1.245
3	.834	8.156	7.507
4	-.384	-3.721	-3.425
5	.745	-5.233	-4.817
6	-.863	-.579	-.533

10 - FACTORED MOMENTS & REACTIONS

Calculated as (1.40D + 1.70L + 1.00 secondary moment effects)

10.1 FACTORED DESIGN MOMENTS (Tm)

SPAN	<----- left* ----->		<----- midspan ----->		<----- right* ----->	
	max	min	max	min	max	min
1	-20.21	-20.21	24.76	24.76	-44.86	-44.86
2	-34.65	-34.65	2.03	2.03	-75.86	-75.86
3	-137.31	-137.31	88.75	88.75	-143.53	-143.53
4	-115.72	-115.72	57.60	57.60	-87.34	-87.34
5	-53.38	-53.38	4.66	4.66	-.99	-.99

Note:

* = Centerline

10.2 SECONDARY MOMENTS (Tm)

SPAN	<--- left* --->		<--- midspan --->		<--- right* --->	
	max	min	max	min	max	min
1	10.39	3.51	-1.37			
2	-5.97	-6.92	-7.86			
3	7.80	10.66	13.52			
4	6.38	6.93	7.49			
5	-2.56	-.72	1.11			

Note:

* = Centerline

10.3 FACTORED REACTIONS (T)

JOINT	max	min	10.4 FACTORED COLUMN MOMENTS (Tm)		<--- LOWER column --->		<--- UPPER column --->	
	max	min	max	min	max	min	max	min
1	35.88	29.32	-1.80	-1.57	-7.18	-9.69		
2	77.50	64.59	5.32	4.71	4.89	3.84		
3	127.29	105.65	5.12	31.99	-23.13	-29.45		
4	150.95	125.67	14.47	11.36	13.32	10.46		
5	106.33	88.26	17.69	13.77	16.28	12.67		
6	17.63	14.47	.52	.33	.47	.30		

11 - MILD STEEL

Support cut-off length for minimum steel(length/span)17
 Span cut-off length for minimum steel(length/span)33
 Top bar extension beyond where required 30.00 cm
 Bottom bar extension beyond where required 30.00 cm

REINFORCEMENT based on NO REDISTRIBUTION of factored moments

11.1 TOTAL WEIGHT OF REBAR = 51.0 Kg AVERAGE = .2 Kg/m²
 TOTAL AREA COVERED = 259.51 m²

11.2.1 STEEL AT MID-SPAN

SPAN	TOP					BOTTOM				
	As (cm ²)	DIFFERENT REBAR CRITERIA			As (cm ²)	DIFFERENT REBAR CRITERIA			As (cm ²)	
		<---ULT	<---TENS	<---TENS		<---ULT	<---TENS	<---TENS		
1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
3	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

11.3.1 STEEL AT SUPPORTS

JOINT	T O P					B O T T O M				
	As (cm ²)	DIFFERENT REBAR CRITERIA				As (cm ²)	DIFFERENT REBAR CRITERIA			
		<---ULT	---MIN---	---	>---		<---ULT	---MIN---	---	>---
1	2	3	4	5	6	7	8	9		
1	.0	(	.0	.0	.0)	.0	(	.0	.0	.0)
2	.0	(	.0	.0	.0)	.0	(	.0	.0	.0)
3	14.4	(	14.4	.0	.0)	.0	(	.0	.0	.0)
4	29.6	(	29.6	.0	.0)	.0	(	.0	.0	.0)
5	11.1	(	11.1	.0	.0)	.0	(	.0	.0	.0)
6	.0	(	.0	.0	.0)	.0	(	.0	.0	.0)

11.2.2 & 11.3.2 LISTING OF THE ENTIRE PROVIDED REBAR

SPAN	ID	LOCATION	NUM	BAR	LENGTH [cm]	AREA [cm ²]
1	2	3	4	5	6	7
3	1	T	21 #	3 x	60	14.9
3	2	T	42 #	3 x	60	29.8
4	3	T	16 #	3 x	60	11.4

Notes:

Bar location - T = Top, B = Bottom.

NUM - Number of bars.

For two-way systems a minimum of 4 bars is specified over the supports.
Refer to tables 11.5.1, 11.5.2 and PTsum graphical display for positioning of bars.

11.5.1 ARRANGEMENT OF TOP BARS

SPAN	T O P S T E E L				
	ID	LOCATION	NUM	BAR	LENGTH [cm]
1	2	3	4	5	6
3	1	LEFT	21 #	3 x	60
3	2	RIGHT	42 #	3 x	60
4	3	RIGHT	16 #	3 x	60

11.5.2 ARRANGEMENT OF BOTTOM BARS

SPAN	B O T T O M S T E E L				
	ID	LOCATION	NUM	BAR	LENGTH [cm]
1	2	3	4	5	6

12 - PUNCHING SHEAR CHECK

LEGEND:

CONDITION... 1 = INTERIOR COLUMN
 2 = END COLUMN
 3 = CORNER COLUMN
 4 = EDGE COLUMN (PARALLEL TO SPAN)
 5 = EDGE BEAM WALL, OR OTHER NON-CONFORMING GEOMETRY
 6 = STRIP TOO NARROW TO DEVELOP PUNCHING SHEAR
 PERFORM SHEAR CHECK MANUALLY

CASE..... 1 = STRESS WITHIN SECTION #1 GOVERNS (COL.CAP OR SLAB)
 2 = STRESS WITHIN SECTION #2 GOVERNS (DROP PANEL OR SLAB)

JNT	COND.	FACTORED ACTIONS		<- PUNCHING SHEAR STRESSES IN kg/cm ² ->		TOTAL	allow- able	STRESS RATIO	CASE
		shear	moment	due to shear	due to moment				
1	2	3	4	5	6	7	8	9	10
1	5	-----	-----	-----	-----	-----	-----	-----	---
2	5	-----	-----	-----	-----	-----	-----	-----	---
3	5	-----	-----	-----	-----	-----	-----	-----	---
4	5	-----	-----	-----	-----	-----	-----	-----	---
5	5	-----	-----	-----	-----	-----	-----	-----	---
6	2	17.63	.99	2.17	.32	2.49	10.65	.23	1

PUNCHING SHEAR CHECK NOT CARRIED OUT FOR SUPPORT WITH CONDITIONS 5 OR 6

13 - MAXIMUM SPAN DEFLECTIONS

Concrete's modulus of elasticity Ec = 274.64 T/cm²

Creep factor K = 2.00
 Ieffective/Igross...(due to cracking)..... K = 1.00

where stresses exceed $1.616(f_c')^{1/2}$ cracking of section is allowed for.
 Values in parentheses are (span/max deflection) ratios

SPAN	<.....DEFLECTION ARE ALL IN CM , DOWNWARD POSITIVE.....>				
	DL	DL+PT	DL+PT+CREEP	LL	DL+PT+LL+CREEP
1	.1	.0	.0(11589)	.0(51765)	.1(9469)
2	.0	-.1	-.2(3295)	.0(*****)	-.2(3212)
3	.9	.3	1.0(1108)	.2(7581)	1.2(967)
4	.4	.1	.4(2610)	.1(14993)	.4(2223)
5	.0	.0	-.1(6214)	.0(*****)	-.1(6028)

ตัวอย่าง

15 - REINFORCEMENT DUE TO MOMENTS FROM LATERAL FORCES

- o Lateral moments are considered with positive and reversed directions
 o Percentage of post-tensioning considered in resisting lateral moments = 70 %
 o Number of strands considered for moment transfer to columns = 19
 o Factored moments calculated are the larger from the followings equations
 i) $M_u = (1.05M_d + 1.28M_l + 1.00M_{sec} + 1.28M_{lat})$
 ii) $M_u = (.90M_d + .00M_l + 1.00M_{sec} + 1.30M_{lat})$
 where, M_d = dead load moments;
 M_l = live load moments;
 M_{sec} = secondary moments; and
 M_{lat} = lateral moments.

15.1 INPUTTED LATERAL MOMENTS AND THE RESULTING COMBINED MOMENTS M_u

<- I N P U T ->			<----- CALCULATED FACTORED SPAN MOMENTS M_u ----->					
LATERAL MOMENTS			LEFT		MID-SPAN		RIGHT	
span	left	right	neg	pos	neg	pos	neg	pos
-1-----2-----3-----4-----5-----6-----7-----8-----9-----								
1	12.76	-13.93	-28.91	10.67	.00	20.20	-52.34	.00
2	13.93	-24.71	-45.32	.00	-9.15	6.70	-90.53	.00
3	12.35	-21.04	-116.91	.00	.00	74.83	-131.28	.00
4	25.25	-8.27	-117.58	.00	.00	55.83	-74.27	.00
5	18.13	-16.31	-63.91	.00	.00	4.48	-21.34	21.20

Note: Moments listed under 4,5,8,9 are reduced to face-of-support, if applicable.
 For distribution of moments see file LATBM.DAT

15.2 COLUMN MOMENTS AND MOMENTS TO BE TRANSFERRED OVER LIMITED SLAB/BEAM WIDTH

<--- GAMMA*(UNBALANCED JOINT MOMENT) --->								
LEFT			RIGHT			MAX	MU	PT
JNT	GAMMA	neg	pos	neg	pos	neg	pos	T
-1-----2-----3-----4-----5-----6-----7-----8-----9-----								
1	1.00	.00	.00	-28.91	10.67	-28.91	10.67	216.32
2	1.00	-42.67	.00	-31.99	.00	-31.99	42.67	216.32
3	1.00	-22.76	.00	-89.64	.00	-89.64	22.76	216.32
4	1.00	-78.34	.00	-48.70	.00	-48.70	78.34	216.32
5	1.00	-56.78	.00	-20.92	.00	-20.92	56.78	216.32
6	.77	-16.54	16.43	.00	.00	-21.20	21.34	216.32

Note: Moments listed under 3,4,5,6 are reduced to face-of-support, if applicable.
 Values in columns 7 and 8 are the sum of lower and upper column moments.
 GAMMA = Fraction of moment taken by flexure of a limited slab width (ACI-318)
 PT = PT force assumed available to resist the unbalanced moment

15.3 LEGENDS AND NOTES FOR MILD STEEL

Columns 2 and the like in following block list total rebar
 due to lateral forces. These are not in addition to other
 considerations reported in preceding blocks.
 For details of rebar reinforcement refer to file LATSTL.DAT

15.4 NO added MILD REINFORCEMENT is required at MID-SPAN

15.5 SELECTION OF REBAR AT S U P P O R T S

<----- T O P S T E E L ----->					<----- B O T T O M S T E E L ----->				
JNT	(cm ²)	Ult	Trans	SELECTION	(cm ²)	Ult	Trans	SELECTION	
-1-----2-----3-----4-----5-----6-----7-----8-----9-----									
1									
2									
3	32.4	(32.4	21.6)	46 # 3 x	146 cm	.0			
4	52.6	(52.6	11.6)	75 # 3 x	269 cm	.0			
5	19.7	(19.7	.0)	28 # 3 x	150 cm	.0			
6									

16 - FRICTION, ELONGATION AND LONG TERM STRESS LOSSES

16.6 LONG TERM STRESS LOSS CALCULATIONS

16.6.1 INPUT PARAMETERS :

Type of strand	LOW LAX	
Modulus of elasticity of strand	2040.00	T/cm ²
Average weight of concrete	NORMAL	
Estimate age of concrete at stressing	3	days
Modulus of elasticity of concrete at stressing	108.00	T/cm ²
Modulus of elasticity of concrete at 28 days	274.64	T/cm ²
Estimate of average relative humidity	80.00	%
Volume to surface ratio of member	15.00	cm

16.6.2 CALCULATED LONG-TERM STRESS LOSS(average of all tendons) :

SPAN	start	center	right
1	.52	.57	.63
2	.64	.64	.71
3	.66	.59	.68
4	.68	.57	.57
5	.59	.54	.52

16.7 FRICTION AND ELONGATION CALCULATIONS

16.7.1 INPUT PARAMETERS :

Coefficient of angular friction (mu)	.250	rad
Coefficient of wobble friction (K)	.0060	/
Ultimate strength of strand	.770	T/cm ²
Ratio of jacking stress to strand's ultimate strength	.600	cm
Anchor set	.990	cm ²

16.7.2 CALCULATED STRESSES(average of all tendons) :

SPAN	LENGTH m	P	start	center	right	X1/L	X2/L	start	center	right
1	5.70	1	15.0	9.2	23.7	.10	.50	10.86	11.32	12.06
2	5.70	1	23.7	14.2	24.7	.10	.50	12.06	11.97	11.31
3	11.40	1	24.7	4.2	23.7	.10	.50	11.29	11.20	11.58
4	9.50	1	23.7	4.2	23.7	.10	.50	11.20	12.08	11.76
5	4.25	1	23.7	13.2	15.0	.10	.50	11.74	11.05	10.78

Note: P= tendon profile (refer to legend of data block 9)
Stresses at each location are the average of strands after anchor set,
and after long-term losses

16.8 TENDON SELECTION AND DATA

TYPE	OFF	FORCE	STRESS RATIO	ELONGATION	STRESS RATIO
			ANCH.	MAX.	
1	2	3	4	5	6
A	21	11.30	19.5	2.0	.67
B	13	11.83	7.1	.0	.68

Note: Force is the average value per strand (T)
Stress ratios are at anchorage (7) and maximum along tendon (8)

POSTEN ENGINEERING CO., LTD.
39/147 POSTEN HOUSE BLDG. LARD PRAO 23, RATCHADHA-PHISEK RD., LARD YAO,
JATUJAK, BANGKOK 10900 Tel. 9390152-6 Fax. 9390157

ADAPT-PT FOR POST-TENSIONED BEAM/SLAB DESIGN
Version 7.00 AMERICAN (ACI 318-99/UBC-77)
ADAPT CORPORATION - Structural Concrete Software System
1733 Woodside Road, Suite 220, Redwood City, California 94061
Phone: (650)306-2400, Fax: (650)364-4678
Email: Support@AdaptSoft.com, Web site: http://www.AdaptSoft.com

DATE AND TIME OF PROGRAM EXECUTION: Apr 5, 2024 At Time: 9:15
PROJECT FILE: 19TH-C(Z-1)

PROJECT TITLE:
VEHHA HUAHIN
19TH-C(Z-1)

2 - INPUT GEOMETRY

2.1.1 PRINCIPAL SPAN DATA OF UNIFORM SPANS

S	T	F	LENGTH	WIDTH	DEPTH	TOP FLANGE	BOTTOM/MIDDLE FLANGE	REF	MULTIPLIER
P	Y	O				width thick.	width thick.	HEIGHT	left right
A	P	R				cm	cm	cm	
N	E	M	m	cm	cm	cm	cm	cm	
1	2	3	4	5	6	7	8	9	10
C	N	1	5.70	650.00	45.00			25.00	.29 .71
1	N	1	7.40	670.00	22.00			22.00	.29 .71

LEGEND:

1 - SPAN
C = Cantilever
2 - TYPE
U = Uniform; prismatic
N = Nonuniform section

3 - FORM
1 = Rectangular section
2 = T or Inverted L section
3 = I section
7 = Joist
8 = Waffle
11 - Top surface to reference line

2.1.2 DETAILED DATA FOR NONUNIFORM SPANS

The following are geometry of nonuniform spans and/or cantilevers.
Left distance is from left support centerline to start of a span segment.

S	F	LEFT	WIDTH	DEPTH	TOP FLANGE	BOTTOM/MIDDLE FLANGE	REF	MULTIPLIER
E	R	DISTANCE			width thick.	width thick.	HEIGHT	left right
G	M	m	cm	cm	cm	cm	cm	
1	2	3	4	5	6	7	8	9
CANTILEVER LEFT								
1	1	.00	650.00	45.00			25.00	.29 .71
2	1	3.20	650.00	25.00			25.00	.29 .71
3	1	4.00	650.00	22.00			22.00	.29 .71
SPAN: 1								
1	1	.00	670.00	45.00			25.00	.29 .71
2	1	.25	670.00	45.00			25.00	.29 .71
3	1	1.15	670.00	22.00			22.00	.29 .71
4	1	7.15	670.00	22.00			22.00	.29 .71

2.2 - SUPPORT WIDTH AND COLUMN DATA

SUPPORT		LOWER COLUMN				UPPER COLUMN			
JOINT	WIDTH	LENGTH	B(DIA)	D	CBC*	LENGTH	B(DIA)	D	CBC*
	cm	m	cm	cm		m	cm	cm	
1	.00	3.25	100.00	50.00	(1)	3.25	100.00	50.00	(1)
2	.00	3.25	220.00	50.00	(1)	3.25	220.00	50.00	(1)

*THE COLUMN BOUNDARY CONDITION CODES (CBC)

Fixed at both ends ... (STANDARD) = 1
Hinged at near end, fixed at far end = 2
Fixed at near end, hinged at far end = 3
Fixed at near end, roller with rotational fixity at far end .. = 4

3 - INPUT APPLIED LOADING

<---CLASS--->

D = DEAD LOAD

L = LIVE LOAD

<-----TYPE----->

U = UNIFORM

C = CONCENTRATED

Li = LINE LOAD

P = PARTIAL UNIFORM

M = APPLIED MOMENT

SW= SELF WEIGHT Computed from geometry input and treated as dead loading
 Unit selfweight $w = 2400.0 \text{ Kg/m}^3$

SPAN	CLASS	TYPE	Intensity T/m^2	(From ... m	To) m	(M or C ...At) T-m or T ...m	Total on Trib T/m	
-1	-2	-3	-4	-5	-6	-7	-8	-9
CANT	L	U	.200	.00	3.20			1.300
CANT	L	U	.200	3.20	4.00			1.300
CANT	L	U	.200	4.00	5.70			1.300
CANT	D	U	.400	.00	3.20			2.600
CANT	D	U	.400	3.20	4.00			2.600
CANT	D	U	.400	4.00	5.70			2.600
CANT	SW	P		.00	3.20			7.020
CANT	SW	P		3.20	4.00			3.900
CANT	SW	P		4.00	5.70			3.432
1	L	U	.200	.00	.25			1.340
1	L	U	.200	.25	1.15			1.340
1	L	U	.200	1.15	7.15			1.340
1	L	U	.200	7.15	7.40			1.340
1	D	U	.400	.00	.25			2.680
1	D	U	.400	.25	1.15			2.680
1	D	U	.400	1.15	7.15			2.680
1	D	U	.400	7.15	7.40			2.680
1	SW	P		.00	.25			7.236
1	SW	P		.25	1.15			7.236
1	SW	P		1.15	7.15			3.538
1	SW	P		7.15	7.40			3.538

3.1 - LOADING AS APPEARS IN USER'S INPUT SCREEN FOR TO PROCESSING

			UNIFORM (T/m ²) LINE (T/m)	(CON. o (T@m)	PART. (m-m)	(M O M E N T) (T-m @ m)
SPAN	CLASS	TYPE				
-1	-2	-3	-4	-5	-6	-7
CANT	L	U	.200			
CANT	D	U	.400			
1	L	U	.200			
1	D	U	.400			

NOTE: SELFWEIGHT INCLUSION REQUIRED

5 - DEAD LOAD MOMENTS, SHEARS & REACTIONS

SPAN	< 5.1 SPAN M(l)*	MOMENTS Midspan	(Tm) M(r)*	> 5.2 SPAN SHEARS SH(l)	(T) SH(r)
-1	-2	-3	-4	-5	-6
CANT					
1	-64.08	5.51	-117.71 -12.46	-33.90	46.24 16.36

Note:

* = Centerline moments

JOINT	< 5.3 REACTIONS (T)	>	<- 5.4 COLUMN MOMENTS (Tm)	->
-1	-2	-3	-4	-5
1	80.14		28.50	25.13
2	16.36		6.42	6.04

6 - LIVE LOAD MOMENTS, SHEARS & REACTIONS

-- 6.1 LIVE LOAD SPAN MOMENTS (Tm) and SHEAR FORCES (T) -->							
SPAN	<---- left* ---->		<--- midspan --->		<---- right* ---->		<--SHEAR FORCE-->
	max	min	max	min	max	min	left right

-1-----2-----3-----4-----5-----6-----7-----8-----9--										
CL										
1	-12.40	-12.40	1.43	1.43	-21.12	-3.08	-3.08	-6.22	7.41	3.70

Note:

* = Centerline moments

<- 6.2 REACTIONS (T) ->			6.3 COLUMN MOMENTS (Tm)			
			<--- LOWER COLUMN --->		<--- UPPER COLUMN --->	
JOINT	max	min	max	min	max	min
-1-----2-----3-----4-----5-----6-----7-----						
1	13.63	.00	4.63	.00	4.08	.00
2	3.70	.00	1.59	.00	1.49	.00

Note: Block 6.1 through 6.3 values are maxima of all skipped loading cases

8 - SUM OF DEAD AND LIVE MOMENTS (Tm)

Maxima of dead load and live load span moments combined
for serviceability checks (1.00DL + 1.00LL)

<----- left* ----->		<----- midspan ----->		<----- right* ----->		
SPAN	max	min	max	min	max	min
-1-----2-----3-----4-----5-----6-----7-----						
CL					-138.82	
1	-76.48	-76.48	6.94	6.94	-15.54	-15.54

Note:

* = Centerline

8 - SUM OF DEAD AND LIVE MOMENTS (Tm)

Maxima of dead load and live load span moments combined
for serviceability checks (1.00DL + 1.00LL)

	<----- left* ----->		<----- midspan ----->		<----- right* ----->	
SPAN	max	min	max	min	max	min
-1-----2-----3-----4-----5-----6-----7-----						
CL					-138.82	
1	-76.48	-76.48	6.94	6.94	-15.54	-15.54

Note:

* = Centerline

9 - SELECTED POST-TENSIONING FORCES AND TENDON PROFILES

9.1 PROFILE TYPES AND PARAMETERS

LEGEND:

For Span:

- 1 = reversed parabola
- 2 = simple parabola with straight portion over support
- 3 = harped tendon

For Cantilever:

- 1 = simple parabola
- 2 = partial parabola
- 3 = harped tendon

9.2 TENDON PROFILE					
TYPE	X1/L	X2/L	X3/L	A/L	
-1-----2-----3-----4-----5-----					
CANT			.439		
1	2	.088	.544	.000	.000

9.3 - SELECTED POST-TENSIONING FORCES AND TENDON DRAPE

Tendon editing mode selected: TENDON SELECTION

	<----- SELECTED VALUES ----->			<--- CALCULATED VALUES --->			
	FORCE	<- DISTANCE OF CGS (cm) ->			P/A	wbal	wbal
SPAN	(T/-)	Left	Center	Right	(Kg/cm^2)	(T/-)	(%DL)
	2	3	4	5	6	7	8
---	1-----	2-----	3-----	4-----	5-----	6-----	7-----
CANT	336.958	11.00		20.65	11.54	3.575	44

1	251.460	20.70	7.20	11.00	17.02	3.476	51
---	---------	-------	------	-------	-------	-------	----

Approximate weight of strand 277.0 Kg

9.35 - TENDON SELECTION DATA:

TYPE	SEL.	FORCE (T)	TENDON EXTENTS
-1	2	3	<C> <1>
A	3	11.78	=====
B	18	11.72	<=====
C	9	11.15	<==

9.5 REQUIRED MINIMUM POST-TENSIONING FORCES (T)

SPAN	<- BASED ON STRESS CONDITIONS ->			<- BASED ON MINIMUM P/A ->		
	LEFT*	CENTER	RIGHT*	LEFT	CENTER	RIGHT
-1	2	3	4	5	6	7
CANT			311.20			277.88
1	.00	.00	.00	286.43	140.03	140.03

Note:

* = Centerline

9.6 SERVICE STRESSES (Kg/cm²)(tension shown positive)

SPAN	LEFT*		CENTER		RIGHT*	
	TOP	BOTTOM	TOP	BOTTOM	TOP	BOTTOM
-1	2	3	4	5	6	7
CANT					23.07	-47.6
1	-3.51	-20.20	-17.68	-16.44	-10.95	-2.22

Note:

* = Centerline

9.7 POST-TENSIONING BALANCED MOMENTS, SHEARS & REACTIONS

SPAN	<-- SPAN MOMENTS (Tm) -->			<-- SPAN SHEARS (T) -->	
	left*	midspan	right*	SH(l)	SH(r)
-1	2	3	4	5	6
CANT			61.78		.00
1	50.41	-6.61	1.79	1.67	-1.67

Note:

* = Centerline

-joint	<-- REACTIONS (T) -->		<-- COLUMN MOMENTS (Tm) -->	
	1	2	Lower columns	Upper columns
1	1.671	-5.154	-5.090	
2	-1.671	-4.530	-4.264	

10 - FACTORED MOMENTS & REACTIONS

Calculated as (1.40D + 1.70L + 1.00 secondary moment effects)

10.1 FACTORED DESIGN MOMENTS (Tm)

SPAN	<---- left* ---->		<---- midspan ---->		<---- right* ---->	
	max	min	max	min	max	min
-1	2	3	4	5	6	7
CL					-200.68	
1	-121.65	-121.65	9.11	9.11	-13.89	-13.89

Note:

* = Centerline

10.2 SECONDARY MOMENTS (Tm)

SPAN	<-- left* -->	<-- midspan -->	<-- right* -->
-1	2	3	4
1	-10.86	-1.03	8.79

Note:

* = Centerline

10.3 FACTORED REACTIONS (T)			10.4 FACTORED COLUMN MOMENTS (Tm)			
JOINT			<--- LOWER column --->		<--- UPPER column --->	
	max	min	max	min	max	min
1	137.04	113.87	42.00	34.13	37.03	30.09
2	27.52	21.23	7.15	4.46	6.73	4.19

11 - MILD STEEL

Support cut-off length for minimum steel(length/span)17
 Span cut-off length for minimum steel(length/span)33
 Top bar extension beyond where required 30.00 cm
 Bottom bar extension beyond where required 30.00 cm

REINFORCEMENT based on NO REDISTRIBUTION of factored moments

11.1	TOTAL WEIGHT OF REBAR =	31.8	Kg	AVERAGE =	.4	Kg/m ²
	TOTAL AREA COVERED =	86.63	m ²			

11.2.1 STEEL AT MID-SPAN									
SPAN	TOP		DIFFERENT REBAR CRITERIA		SPAN	BOTTOM		DIFFERENT REBAR CRITERIA	
	AS (cm ²)	<---ULT---TENS--->	AS (cm ²)	<---ULT---TENS--->		AS (cm ²)	<---ULT---TENS--->	AS (cm ²)	<---ULT---TENS--->
1	.0	(.0 .0 .0 .0)	.0	(.0 .0 .0 .0)	1	.0	(.0 .0 .0 .0)	.0	(.0 .0 .0 .0)

11.3.1 STEEL AT SUPPORTS									
JOINT	TOP		DIFFERENT REBAR CRITERIA		JOINT	BOTTOM		DIFFERENT REBAR CRITERIA	
	AS (cm ²)	<---ULT---MIN--->	AS (cm ²)	<---ULT---MIN--->		AS (cm ²)	<---ULT---MIN--->	AS (cm ²)	<---ULT---MIN--->
1	6.3	(6.3 .0 .0)	.0	(.0 .0 .0)	1	.0	(.0 .0 .0)	.0	(.0 .0 .0)
2	.0	(.0 .0 .0)	.0	(.0 .0 .0)	2	.0	(.0 .0 .0)	.0	(.0 .0 .0)

11.2.2 & 11.3.2 LISTING OF THE ENTIRE PROVIDED REBAR

SPAN	ID	LOCATION	NUM	BAR	LENGTH [cm]	REA [cm ²]
0	1	T	9 #	3 x	60	6.3

Notes:

Bar location - T = Top, B = Bottom.

NUM - Number of bars.

For two-way systems a minimum of 4 bars is specified over the supports.
 Refer to tables 11.5.1, 11.5.2 and PTsum graphical display for positioning of bars.

11.5.1 ARRANGEMENT OF TOP BARS

TOP STEEL					
SPAN	ID	LOCATION	NUM	BAR	LENGTH [cm]
0	1	RIGHT	9 #	3 x	60

11.5.2 ARRANGEMENT OF BOTTOM BARS

BOTTOM STEEL					
SPAN	ID	LOCATION	NUM	BAR	LENGTH [cm]
1	2				

12 - PUNCHING SHEAR CHECK

LEGEND:

CONDITION... 1 = INTERIOR COLUMN
 2 = END COLUMN
 3 = CORNER COLUMN
 4 = EDGE COLUMN (PARALLEL TO SPAN)
 5 = EDGE BEAM, WALL, OR OTHER NON-CONFORMING GEOMETRY
 PERFORM SHEAR CHECK MANUALLY
 6 = STRIP TOO NARROW TO DEVELOP PUNCHING SHEAR

CASE..... 1 = STRESS WITHIN SECTION #1 GOVERNS (COL.CAP OR SLAB)
 2 = STRESS WITHIN SECTION #2 GOVERNS (DROP PANEL OR SLAB)

JNT	COND.	FACTORED ACTIONS		<- PUNCHING SHEAR STRESSES IN Kg/cm ² ->		TOTAL	allow- able	STRESS RATIO	CASE
		shear T	moment T-m	due to shear	due to moment				
-1-	-2-	-3-	-4-	-5-	-6-	-7-	-8-	-9-	-10-
1	4	137.04	79.03	10.05	5.59	15.64	16.38	.96	1
2	2	27.52	13.89	4.28	.92	5.20	11.91	.44	1

PUNCHING SHEAR CHECK SATISFACTORY
 NO ADDITIONAL REBAR OR CHANGE IN SECTION IS NECESSARY

13 - MAXIMUM SPAN DEFLECTIONS

Concrete's modulus of elasticity $E_c = 274.64 \text{ T/cm}^2$
 Creep factor $K = 2.00$
 Ieffective/Igross...(due to cracking)..... $K = 1.00$

Where stresses exceed $1.616(f_c')^{1/2}$ cracking of section is allowed for.
 Values in parentheses are (span/max deflection) ratios

SPAN	<.....DEFLECTION ARE ALL IN cm , DOWNWARD POSITIVE.....>			
	DL	DL+PT	DL+PT+LL+CREEP	LL
-1-	-2-	-3-	-4-	-5-
CANL	1.2	.4	1.3(430)	.2(2663)
1	-.1	-.2	-.6(1337)	.0(32948)

15 - REINFORCEMENT DUE TO MOMENTS FROM LATERAL FORCES

=====

o Lateral moments are considered with positive and reversed directions

o Percentage of post-tensioning considered in resisting lateral moments= 80 %

o Number of strands considered for moment transfer to columns = 10

o Factored moments calculated are the larger from the followings equations

i) $M_u = (1.05M_d + 1.28M_l + 1.00M_{sec} + 1.28M_{lat})$

ii) $M_u = (.90M_d + .00M_l + 1.00M_{sec} + 1.30M_{lat})$

where, M_d = dead load moments;

M_l = live load moments;

M_{sec} = secondary moments; and

M_{lat} = lateral moments.

15.1 INPUTTED LATERAL MOMENTS AND THE RESULTING COMBINED MOMENTS M_u

<- I N P U T ->		<----- CALCULATED FACTORED SPAN MOMENTS M_u ----->						
LATERAL MOMENTS		LEFT		MID-SPAN		RIGHT		
span	left	right	neg	pos	neg	pos	neg	pos
-1-----2-----3-----4-----5-----6-----7-----8-----9--								
1	6.34	-3.33	-102.14	.00	.00	8.51	-12.50	1.91

Note: Moments listed under 4,5,8,9 are reduced to face-of-support, if applicable.
For distribution of moments see file LATBM.DAT

15.2 COLUMN MOMENTS AND MOMENTS TO BE TRANSFERRED OVER LIMITED SLAB/BEAM WIDTH

<--- GAMMA*(UNBALANCED JOINT MOMENT) --->		LEFT		RIGHT		MAX COLUMN MOMENT		PT
JNT	GAMMA	neg	pos	neg	pos	neg	pos	T
-1-----2-----3-----4-----5-----6-----7-----8-----9--								
1	.63	.00	.00	.00	.00	.00	64.71	11.85
2	.75	-9.38	1.43	.00	.00	-1.91	12.50	113.85

Note: Moments listed under 3,4,5,6 are reduced to face-of-support, if applicable.
Values in columns 7 and 8 are the sum of lower and upper column moments.

GAMMA = Fraction of moment taken by flexure of a limited slab width (ACI-318)

PT = PT force assumed available to resist the unbalanced moment

15.3 LEGENDS AND NOTES FOR MILD STEEL

Columns 2 and the like in following block list have rebar due to lateral forces. These are not in addition to other considerations reported in preceding blocks.

For details of rebar reinforcement refer to file LATSTL.DAT

15.4-5 NO added MILD REINFORCEMENT is required at MID-SPAN or SUPPORT

16 - FRICTION, ELONGATION AND LONG TERM STRESS LOSSES

16.6 LONG TERM STRESS LOSS CALCULATIONS

16.6.1 INPUT PARAMETERS :

Type of strand	LOW LAX	
Modulus of elasticity of strand	2040.00	T/cm ²
Average weight of concrete	NORMAL	
Estimate age of concrete at stressing	3	days
Modulus of elasticity of concrete at stressing	108.00	T/cm ²
Modulus of elasticity of concrete at 28 days	274.64	T/cm ²
Estimate of average relative humidity	80.00	%
Volume to surface ratio of member	12.50	cm

16.6.2 CALCULATED LONG-TERM STRESS LOSS(average of all tendons) :

SPAN	<----- STRESS (T/cm ²) ----->		
	start	center	right
-1-----2-----3-----4-----			
CANL			.89
1	.77	.79	.75

16.7 FRICTION AND ELONGATION CALCULATIONS

16.7.1 INPUT PARAMETERS :

Coefficient of angular friction (mu)	.250	/rad
Coefficient of wobble friction (K)	.0	/m
Ultimate strength of strand	1770	T/cm ²
Ratio of jacking stress to strand's ultimate strength	.770	
Anchor set	.600	cm
Cross-sectional area of strand	1.5	cm ²

16.7.2 CALCULATED STRESSES(average of all tendons) :

SPAN	LENGTH m	P	<TENDON HEIGHT(cm)>			Horizontal ratios			<-- STRESS(T/cm ²)-->		
			start	center	right	X1/L	X2/L	X3/L	start	center	right
-1-----2-----3-----4-----5-----6-----7-----8-----9-----10-----11-----12-----											
CANL	5.70	2	11.0		20.6			.44			11.37
1	7.40	2	20.7	7.2	11.0	.09	.54		12.2	12.07	11.76

Note: P= tendon profile (refer to legend of data block)
Stresses at each location are the average of strands after anchor set, and after long-term losses

16.8 TENDON SELECTION AND DATA:

TYPE	OFF	FORCE	<----- TENDON EXTENTS ----->			ELONGATION		Stress ratios	
			CAN<-----S P A N S----->CAN			LEFT (cm)	RIGHT (cm)	Anch.	Max.
-1-----2-----3-----4-----5-----6-----7-----8-----									
A	3	11.78	=====			.0	8.1	.66	.70
B	18	11.72	<=====			8.1	.0	.66	.69
C	9	11.15	<====			3.4	.0	.61	.65

Note: Force is the average value per strand (T)
Stress ratios are at average (7) and maximum along tendon (8)

POSTEN ENGINEERING CO., LTD.
39/147 POSTEN HOUSE BLDG. LARD PRAO 23, RATCHADHA-PHISEK RD., LARD YAO,
JATUJAK, BANGKOK 10900 Tel. 9390152-6 Fax. 9390157

ADAPT-PT FOR POST-TENSIONED BEAM/SLAB DESIGN
Version 7.00 AMERICAN (ACI 318-99/UBC-77)
ADAPT CORPORATION - Structural Concrete Software System
1733 Woodside Road, Suite 220, Redwood City, California 94061
Phone: (650)306-2400, Fax: (650)364-4678
Email: Support@AdaptSoft.com, Web site: http://www.AdaptSoft.com

DATE AND TIME OF PROGRAM EXECUTION: Apr 5, 2024 At Time: 8:46
PROJECT FILE: 19TH-B(Z-1)

PROJECT TITLE:
VEHHA HUAHIN
19TH-B(Z-1)

1 - USER SPECIFIED GENERAL DESIGN PARAMETERS

CONCRETE:
STRENGTH at 28 days, for BEAMS/SLABS 320.00 Kg/cm²
for COLUMNS 350.00 Kg/cm²
MODULUS OF ELASTICITY for BEAMS/SLABS 274.64 T/cm²
for COLUMNS 287.23 T/cm²
CREEP factor for deflections for BEAMS/SLABS 2.00
CONCRETE WEIGHT NORMAL
SELF WEIGHT 2400.00 Kg/m³
TENSION STRESS limits (multiple of (f'_c)^{1/2})
At Top 1.500
At Bottom 1.590
COMPRESSION STRESS limits (multiple of (f'_c))
At all locations450
REINFORCEMENT:
YIELD Strength 4200 T/cm²
Minimum Cover at TOP 3.00 cm
Minimum Cover at BOTTOM 3.00 cm
POST-TENSIONING:
SYSTEM BONDED
Ultimate strength of strand 19.00 T/cm²
Average effective stress in strand (final) 11.50 T/cm²
Strand area990 cm²
Min CGS of tendon from TOP 4.35 cm
Min CGS of tendon from BOTTOM for INTERIOR spans.. 4.15 cm
Min CGS of tendon from BOTTOM for EXTERIOR spans.. 4.15 cm
Min average precompression 9.50 Kg/cm²
Max spacing between strands (factor of slab depth) 8.00
Tendon profile type and support widths..... (see section 9)
ANALYSIS OPTIONS USED:
Structural system(using EQUIVALENT FRAME).... TWO-WAY

2 - INPUT GEOMETRY

2.1.1 PRINCIPAL SPAN DATA OF UNIFORM SPANS

S P A N N E M	T Y P E	F L A N G E	L E N G T H m	W I D T H cm	D E P T H cm	T O P F L A N G E		B O T T O M / M I D D L E F L A N G E		R E F H E I G H T cm	M U L T I P L I C A T I O N	
						width	thick.	width	thick.		left	right
1	2	3	4	5	6	7	8	9	10	11	12	13
C	N	1	3.90	740.00	45.00					25.00	.35	.65
1	N	1	7.60	740.00	25.00					25.00	.35	.65
2	U	1	7.60	740.00	25.00					25.00	.35	.65
3	N	1	7.60	740.00	25.00					25.00	.45	.55

LEGEND:

1 - SPAN
C = Cantilever
2 - TYPE
U = Uniform; prismatic
N = Nonuniform section

3 - FORM

1 = Rectangular section
2 = T or Inverted L section
3 = I section
4 = Extended T or L section
7 = Joist

8 = Waffle
11 - Top surface to reference line

2.1.2 DETAILED DATA FOR NONUNIFORM SPANS

The following are geometry of nonuniform spans and/or cantilevers.
Left distance is from left support centerline to start of a span segment.

S	F	LEFT	WIDTH	DEPTH	TOP	BOTTOM/MIDDLE	REF	MULTIPLIER			
E	O	DISTANCE			FLANGE	FLANGE	HEIGHT	left right			
G	M	m	cm	cm	width thick.	width thick.	cm				
-1-	-2-	-4-	-5-	-6-	-7-	-8-	-9-	-10-	-11-	-12-	-13-
CANTILEVER LEFT											
1	1	.00	740.00	45.00			25.00	.35	.65		
2	1	2.50	740.00	25.00			25.00	.35	.65		
SPAN: 1											
1	1	.00	740.00	45.00			25.00	.35	.65		
2	1	.17	740.00	45.00			25.00	.35	.65		
3	1	1.30	740.00	25.00			25.00	.35	.65		
4	1	7.43	740.00	25.00			25.00	.35	.65		
SPAN: 3											
1	1	.00	740.00	25.00			25.00	.45	.55		
2	1	.22	740.00	25.00			25.00	.45	.55		
3	1	6.60	740.00	30.00			25.00	.45	.55		
4	1	7.38	740.00	30.00			25.00	.45	.55		

2.2 - SUPPORT WIDTH AND COLUMN DATA

JOINT	SUPPORT	<-----	LOWER COLUMN	>-----		<-----	UPPER COLUMN	>-----	
	WIDTH	LENGTH	B (DIA)	D	CBC*	LENGTH	B (DIA)	D	CBC*
	cm	m	cm	cm		m	cm	cm	
-1-	-2-	-3-	-4-	-5-	-6-	-7-	-8-	-9-	-10-
1	.00	3.25	250.00	35.00	(1)	3.25	250.00	35.00	(1)
2	.00	3.25	400.00	35.00	(1)	3.25	400.00	35.00	(1)
3	.00	3.25	400.00	45.00	(1)	3.25	400.00	45.00	(1)
4	.00	3.25	400.00	45.00	(1)	3.25	400.00	45.00	(1)

*THE COLUMN BOUNDARY CONDITION CODES (CBC)

Fixed at both ends ... (STANDARD) = 1
Hinged at near end, fixed at far end = 2
Fixed at near end, hinged at far end = 3
Fixed at near end, roller with rotational fixity at far end .. = 4

3 - INPUT APPLIED LOADING

<---CLASS---> <-----TYPE----->
D = DEAD LOAD U = UNIFORM P = PARTIAL UNIFORM
C = CONCENTRATED M = APPLIED MOMENT
L = LIVE LOAD Li = LINE LOAD

SW= SELF WEIGHT Computed from geometry input and treated as dead loading
Unit selfweight w = 2400.0 kg/m³

SPAN	CLASS	TYPE	Intensity	(From ...	To)	(M or C ...At)	Total	on Trib
			T/m ²	(m	m)	(T-m or T ...m)		T/m
-1-	-2-	-3-	-4-	-5-	-6-	-7-	-8-	-9-
CANT	L	U	.200	.00	2.50			1.480
CANT	L	U	.200	2.50	3.90			1.480
CANT	D	U	.400	.00	2.50			2.960
CANT	D	U	.400	2.50	3.90			2.960
CANT	SW	P		.00	2.50			7.992
CANT	SW	P		2.50	3.90			4.440
1	L	U	.200	.00	.17			1.480
1	L	U	.200	.17	1.30			1.480
1	L	U	.200	1.30	7.43			1.480
1	L	U	.200	7.43	7.60			1.480
1	D	U	.400	.00	.17			2.960
1	D	U	.400	.17	1.30			2.960
1	D	U	.400	1.30	7.43			2.960

1	D	U	.400	7.43	7.60	2.960
1	SW	P		.00	.17	7.992
1	SW	P		.17	1.30	7.992
1	SW	P		1.30	7.43	4.440
1	SW	P		7.43	7.60	4.440
2	L	U	.200	.00	7.60	1.480
2	D	U	.400	.00	7.60	2.960
2	SW	U		.00	7.60	4.440
3	L	U	.200	.00	.22	1.480
3	L	U	.200	.22	6.60	1.480
3	L	U	.200	6.60	7.38	1.480
3	L	U	.200	7.38	7.60	1.480
3	D	U	.400	.00	.22	2.960
3	D	U	.400	.22	6.60	2.960
3	D	U	.400	6.60	7.38	2.960
3	D	U	.400	7.38	7.60	2.960
3	SW	P		.00	.22	4.440
3	SW	P		.22	6.60	4.440
3	SW	P		6.60	7.38	5.328
3	SW	P		7.38	7.60	5.328

3.1 - LOADING AS APPEARS IN USER'S INPUT SCREEN PRIOR TO PROCESSING

SPAN	CLASS	TYPE	UNIFORM (T/m^2), LINE (T/m)	(CON. or PART.) (T@m or m-m)	(M O M E N T) (T-m @ m)
-1	-2	-3	-4	-5	-6
CANT	L	U	.200		
CANT	D	U	.400		
1	L	U	.200		
1	D	U	.400		
2	L	U	.200		
2	D	U	.400		
3	L	U	.200		
3	D	U	.400		

NOTE: SELFWEIGHT INCLUSION REQUIRED

5 - DEAD LOAD MOMENTS, SHEARS & REACTIONS

SPAN	< 5.1 SPAN M(1)*	MOMENTS Midspan	(Tm) M(1)*	5.2 SPAN SHEARS (T) SH(1)	SH(r)
-1	-2	-3	-4	-5	-6
CANT			67.38		37.74
1	-58.71	11.15	3.84	-36.27	24.58
2	-35.24	16.67	3.28	-27.72	28.52
3	-38.25	18.11	-36.22	-28.45	28.68

Note:

* = Centerline moment

JOINT	< 5.3 REACTIONS (T)	<- 5.4 COLUMN MOMENTS (Tm) ->
-1	-2	-3
1	74.01	4.61
2	52.31	-3.31
3	56.97	.01
4	28.68	18.86

6 - LIVE LOAD MOMENTS, SHEARS & REACTIONS

<-- 6.1 LIVE LOAD SPAN MOMENTS (Tm) and SHEAR FORCES (T) -->

SPAN	<--- left* --->	<--- midspan --->	<--- right* --->	<--- SHEAR FORCE --->
-1	-2	-3	-4	-5
CL			-11.26	
1	-10.60	-10.60	2.38	2.38
2	-7.09	-7.09	3.32	3.32
3	-7.64	-7.64	3.28	3.28

Note:

* = Centerline moments

<- 6.2 REACTIONS (T) ->			6.3 COLUMN MOMENTS (Tm)			
			<--- LOWER COLUMN --->		<--- UPPER COLUMN --->	
JOINT	max	min	max	min	max	min
-1-----2-----3-----4-----5-----6-----7-----						
1	12.00	.00	.35	.00	.31	.00
2	10.57	.00	.00	-.55	.00	-.52
3	11.38	.00	.00	.00	.00	.00
4	5.56	.00	3.74	.00	3.44	.00

Note: Block 6.1 through 6.3 values are maxima of all skipped loading cases.

8 - SUM OF DEAD AND LIVE MOMENTS (Tm)

Maxima of dead load and live load span moments combined
for serviceability checks (1.00DL + 1.00LL)

	<----- left* ----->		<----- midspan ----->		<----- right* ----->	
SPAN	max	min	max	min	max	min
	-----2-----	-----3-----	-----4-----	-----5-----	-----6-----	-----7-----
CL					-78.64	
1	-69.31	-69.31	13.53	13.53	-34.85	-34.85
2	-42.33	-42.33	19.99	19.99	-45.92	-45.92
3	-45.89	-45.89	19.69	19.69	-43.39	-43.39

Note:

* = Centerline

8 - SUM OF DEAD AND LIVE MOMENTS (Tm)

Maxima of dead load and live load span moments combined
for serviceability checks (1.00DL + 1.00LL)

<--- left* --->			<--- midspan --->		<--- right --->	
SPAN	max	min	max	min	max	min
-1-----2-----3-----4-----5-----6-----7-----						
CL					-78.64	
1	-69.31	-69.31	13.53	13.53	-34.85	-34.85
2	-42.33	-42.33	19.99	19.99	-45.92	-45.92
3	-45.89	-45.89	19.69	19.69	-43.39	-43.39

Note:

* = Centerline

9 - SELECTED POST-TENSIONING FORCES AND TENDON PROFILES

9.1 PROFILE TYPES AND PARAMETERS

LEGEND:

For Span:

- 1 = reversed parabola
- 2 = simple parabola with straight portion over support
- 3 = harped tendon

For Cantilever:

- 1 = simple parabola
- 2 = partial parabola
- 3 = harped tendon

9.2	T E N D O N		P R O F I L E		
	TYPE	X1/L	X2/L	X3/L	A/L
	1-----2-----	3-----4-----	5-----		
CANT	2			.436	
1	2	.091	.546	.000	.000
2	1	.100	.500	.100	.000
3	1	.100	.500	.100	.000

9.3 - SELECTED POST-TENSIONING FORCES AND TENDON DRAPE

Tendon editing mode selected: TENDON SELECTION

<----- SELECTED VALUES ----->					<--- CALCULATED VALUES --->		
SPAN	FORCE	<- DISTANCE OF CGS (cm) ->			P/A	wbal	wbal
	(T/-)	Left	Center	Right	(Kg/cm^2)	(T/-)	(%DL)
-1-----	2-----	3-----	4-----	5-----	6-----	7-----	8-----

CANT	303.003	12.00		18.70	9.11	4.741	49
1	242.961	18.70	6.20	18.70	13.20	4.650	58
2	220.731	18.70	4.20	18.70	11.93	4.433	60
3	242.418	18.70	4.20	12.50	13.10	3.828	51

Approximate weight of strand 502.0 kg

9.35 - TENDON SELECTION DATA:

TYPE	SEL.	FORCE (T)	TENDON EXTENTS ----->				
			<C>	<1>	<2>	<3>	
-1-----2-----3-----							
A	20	10.95	=====				
B	8	10.36	<==				
C	4	11.63	=====>				

9.5 REQUIRED MINIMUM POST-TENSIONING FORCES (T)

SPAN	<- BASED ON STRESS CONDITIONS ->			<- BASED ON MINIMUM P/A ->		
	LEFT*	CENTER	RIGHT*	LEFT	CENTER	RIGHT
-1-----2-----3-----4-----5-----6-----7-----						
CANT			33.07			316.35
1	.00	.00	.00	316.35	175.75	175.75
2	.00	.00	.00	175.75	175.75	175.75
3	.00	.00	.00	175.75	175.75	210.90

Note:

* = Centerline

9.6 SERVICE STRESSES (Kg/cm²) (tension shown positive)

SPAN	LEFT *		CENTER		RIGHT *	
	TOP	BOTTOM	TOP	BOTTOM	TOP	BOTTOM
-1-----2-----3-----4-----5-----6-----7-----						
CANT					2.27	21.33
1	-5.62	-13.49	-18.53	-7.74	-9.15	-16.42
2	-6.97	-18.65	-21.86	-2.06	-7.12	-20.70
3	-6.68	-21.15	-24.99	-1.12	6.11	-14.80

Note:

* = Centerline

9.7 POST-TENSIONING BALANCED MOMENTS, SHEARS & REACTIONS

SPAN	<-- SPAN MOMENTS (Tm) -->			<-- SPAN SHEARS (T) -->	
	left*	midspan	right	SH(l)	SH(r)
-1-----2-----3-----4-----5-----6-----					
CANT			17		.00
1	46.90	-9.37	21.58	-.20	-.20
2	21.00	-11.53	21.14	-.03	-.03
3	19.47	0.53	20.54	-1.36	-1.36

Note:

* = Centerline

-joint-----2-----3-----4-----5-----6-----7-----	<-- REACTIONS (T) -->			<-- COLUMN MOMENTS (Tm) -->	
				Lower columns	Upper columns
1	.195			-1.207	-1.064
2	-.163			-.300	-.280
3	1.323			-.862	-.804
4	-1.355			-7.540	-6.940

10 - FACTORED MOMENTS & REACTIONS

calculated as (1.40D + 1.70L + 1.00 secondary moment effects)

10.1 FACTORED DESIGN MOMENTS (Tm)

SPAN	<---- left* ---->		<---- midspan ---->		<---- right* ---->	
	max	min	max	min	max	min
-1-----2-----3-----4-----5-----6-----7-----						
CL					-113.47	
1	-102.49	-102.49	18.13	18.13	-51.38	-51.38
2	-62.75	-62.75	31.23	31.23	-60.73	-60.73

3	-62.36	-62.36	37.89	37.89	-48.42	-48.42
---	--------	--------	-------	-------	--------	--------

Note:

* = Centerline

10.2 SECONDARY MOMENTS (Tm)

SPAN	<-- left* -->	<- midspan ->	<-- right* -->
1	-2.27	-1.53	-.79
2	-1.37	2.24	5.85
3	4.18	9.33	14.48

Note:

* = Centerline

10.3 FACTORED REACTIONS

JOINT	max		min		10.4 FACTORED COLUMN MOMENTS (Tm)	
	max	min	max	min	max	min
1	124.21	103.81	5.83	5.24	5.14	4.62
2	91.04	73.07	-4.93	-5.88	-4.61	-5.49
3	100.43	81.08	-.84	-.84	-.79	-.79
4	48.25	38.80	25.21	18.86	23.21	17.36

11 - MILD STEEL

Support cut-off length for minimum steel(length/span)17
 Span cut-off length for minimum steel(length/span)33
 Top bar extension beyond where required ... 20.00 cm
 Bottom bar extension beyond where required ... 30.00 cm

REINFORCEMENT based on NO REDISTRIBUTION of factored moments

11.1 TOTAL WEIGHT OF REBAR = 6.0 Kg AVERAGE = .0 Kg/m²
 TOTAL AREA COVERED = 197.58 m²

11.2.1 STEEL AT MID-SPAN

SPAN	TOP				BOTTOM			
	As (cm ²)	DIFFERENT REBAR CRITERIA	As (cm ²)	DIFFERENT REBAR CRITERIA	As (cm ²)	DIFFERENT REBAR CRITERIA	As (cm ²)	DIFFERENT REBAR CRITERIA
1	.0	(.0)	.0	(.0)	.0	(.0)	.0	(.0)
2	.0	(.0)	.0	(.0)	.0	(.0)	.0	(.0)
3	.0	(.0)	.0	(.0)	.0	(.0)	.0	(.0)

11.3.1 STEEL AT SUPPORTS

JOINT	TOP				BOTTOM			
	As (cm ²)	DIFFERENT REBAR CRITERIA	As (cm ²)	DIFFERENT REBAR CRITERIA	As (cm ²)	DIFFERENT REBAR CRITERIA	As (cm ²)	DIFFERENT REBAR CRITERIA
1	.0	(.0)	.0	(.0)	.0	(.0)	.0	(.0)
2	7.2	(7.2)	.0	(.0)	.0	(.0)	.0	(.0)
3	.0	(.0)	.0	(.0)	.0	(.0)	.0	(.0)
4	.0	(.0)	.0	(.0)	.0	(.0)	.0	(.0)

11.2.2 & 11.3.2 LISTING OF THE ENTIRE PROVIDED REBAR

SPAN	ID	LOCATION	NUM	BAR	LENGTH [cm]	AREA [cm ²]
2	1	T	11 #	3 x	60	7.8

Notes:

Bar location - T = Top, B = Bottom.

NUM - Number of bars.

For two-way systems a minimum of 4 bars is specified over the supports.
 Refer to tables 11.5.1, 11.5.2 and PTsum graphical display for positioning of bars.

11.5.1 ARRANGEMENT OF TOP BARS

SPAN	ID	LOCATION	NUM	BAR	LENGTH [cm]
2	1	LEFT	11 #	3 x	60

11.5.2 ARRANGEMENT OF BOTTOM BARS

SPAN	BOTTOM STEEL				
	ID	LOCATION	NUM	BAR	LENGTH [cm]
-1-	-2-	3-	4-	5-	6-

12 - PUNCHING SHEAR CHECK

LEGEND:

CONDITION... 1 = INTERIOR COLUMN
 2 = END COLUMN
 3 = CORNER COLUMN
 4 = EDGE COLUMN (PARALLEL TO SPAN)
 5 = EDGE BEAM, WALL, OR OTHER NON-CONFORMING GEOMETRY
 PERFORM SHEAR CHECK MANUALLY
 6 = STRIP TOO NARROW TO DEVELOP PUNCHING SHEAR

CASE..... 1 = STRESS WITHIN SECTION #1 GOVERNS (COL.CAP OR SLAB)
 2 = STRESS WITHIN SECTION #2 GOVERNS (DROP PANEL OR SLAB)

JNT	COND.	FACTORED ACTIONS		<- PUNCHING SHEAR STRESSES IN Kg/cm ² ->		TOTAL	allow- able	STRESS RATIO	CASE
		shear T	moment T-m	due to shear	due to moment				
-1-	2-	3-	4-	5-	6-	7-	8-	9-	10-
1	5	-----	-----	-----	-----	-----	-----	-----	-----
2	5	-----	-----	-----	-----	-----	-----	-----	-----
3	5	-----	-----	-----	-----	-----	-----	-----	-----
4	5	-----	-----	-----	-----	-----	-----	-----	-----

PUNCHING SHEAR CHECK NOT CARRIED OUT FOR SUPPORT WITH CONDITION 5 OR 6

13 - MAXIMUM SPAN DEFLECTIONS

Concrete's modulus of elasticity = 274.4 T/cm²
 Creep factor K = 2.00
 Ieffective/Igross...(due to cracking).... K = 1.00

where stresses exceed $1.616(f_c')^{1/2}$ cracking or section is allowed for.
 Values in parentheses are (span/max deflection) ratios

SPAN	<.....DEFLECTION ARE ALL IN cm.....>				DOWNWARD POSITIVE.....>	
	DL	DL+PT	L+PT+CREEP		DL+PT+LL+CREEP	
-1-	2-	3-	4-	5-	6-	
CANL	.2	.0	-.1(3635)	.0(14054)	.0(12571)	
1	.1	.0	.0(38019)	.0(29525)	.0(16619)	
2	.2	.1	.1(4257)	.0(17805)	.2(3436)	
3	.2	.1	.2(3145)	.0(17797)	.3(2672)	

15 - REINFORCEMENT DUE TO MOMENTS FROM LATERAL FORCES

=====

o Lateral moments are considered with positive and reversed directions

o Percentage of post-tensioning considered in resisting lateral moments= 70 %

o Number of strands considered for moment transfer to columns = 15

o Factored moments calculated are the larger from the followings equations

i) $M_u = (1.05M_d + 1.28M_l + 1.00M_{sec} + 1.28M_{lat})$

ii) $M_u = (.90M_d + .00M_l + 1.00M_{sec} + 1.30M_{lat})$

where, M_d = dead load moments;

M_l = live load moments;

M_{sec} = secondary moments; and

M_{lat} = lateral moments.

15.1 INPUTTED LATERAL MOMENTS AND THE RESULTING COMBINED MOMENTS M_m

span	<- I N P U T -> LATERAL MOMENTS		<----- CALCULATED FACTORED SPAN MOMENTS M_u ----->					
	left	right	LEFT		MID-SPAN		RIGHT	
			neg	pos	neg	pos	neg	pos
1	14.99	-7.80	-96.67	.00	.00	17.83	-48.75	.00
2	7.80	-14.18	-57.42	.00	.00	28.08	-62.27	.00
3	14.18	-19.57	-63.91	.00	.00	34.21	-57.78	7.32

Note: Moments listed under 4,5,8,9 are reduced to face-of-support, if applicable.
For distribution of moments see file LATBM.DAT

15.2 COLUMN MOMENTS AND MOMENTS TO BE TRANSFERRED OVER LIMITED SLAB FLAM WIDTH

JNT	GAMMA	<--- GAMMA*(UNBALANCED JOINT MOMENT) --->				MAX COLUMN MU		PT
		LEFT		RIGHT		neg	pos	
		neg	pos	neg	pos	neg	pos	
1	1.00	.00	.00	-25.92	.00	-25.92	25.86	170.77
2	1.00	-13.94	.00	-28.64	.00	-28.64	13.94	170.77
3	1.00	-35.23	.00	-38.51	.00	-38.51	35.23	170.77
4	1.00	-57.78	7.32	.00	.00	-57.78	57.78	170.77

Note: Moments listed under 3,4,5,6 are reduced to face-of-support, if applicable.
Values in columns 7 and 8 are the sum of lower and upper column moments.
GAMMA = Fraction of moment taken by flexure of a limited slab width (ACI-318)
PT = PT force assumed available to resist the unbalanced moment

15.3 LEGENDS AND NOTES FOR MILD STEEL

Columns 2 and the like in following block list total rebar due to lateral forces. These are in addition to other considerations reported in preceding blocks.
For details of rebar reinforcement refer to file LATSTL.DAT

15.4 NO added MILD REINFORCEMENT IS required at MID-SPAN

15.5 SELECTION OF REBAR AT S U P P O R T S

JNT (cm ²)	<----- T O P S T E E L ----->			<----- B O T T O M S T E E L ----->		
	Ult	Trans	SELECTION	Ult	Trans	SELECTION
1						
2	20.3	(20.3	.0)	29 # 3 x	174 cm	.0
3	24.9	(24.9	.0)	36 # 3 x	212 cm	.0
4	21.3	(20.8	21.3)	30 # 3 x	136 cm	.0

16 - FRICTION, ELONGATION AND LONG TERM STRESS LOSSES

16.6 LONG TERM STRESS LOSS CALCULATIONS

16.6.1 INPUT PARAMETERS :

Type of strand	LOW LAX	
Modulus of elasticity of strand	2040.00	T/cm ²
Average weight of concrete	NORMAL	
Estimate age of concrete at stressing	3	days
Modulus of elasticity of concrete at stressing	108.00	T/cm ²
Modulus of elasticity of concrete at 28 days	274.64	T/cm ²
Estimate of average relative humidity	80.00	%
Volume to surface ratio of member	12.50	cm

16.6.2 CALCULATED LONG-TERM STRESS LOSS(average of all tendons) :

SPAN	<----- STRESS (T/cm ²) ----->		
	start	center	right
-1-----2-----3-----4----			
CANL			.73
1	.69	.71	.67
2	.65	.57	.57
3	.59	.54	.52

16.7 FRICTION AND ELONGATION CALCULATIONS

16.7.1 INPUT PARAMETERS :

Coefficient of angular friction (meu)	.0060	/rad
Coefficient of wobble friction (K)	.0060	
Ultimate strength of strand	1900	T/cm ²
Ratio of jacking stress to strand's ultimate strength	.770	
Anchor set	.600	cm
Cross-sectional area of strand	990	cm ²

16.7.2 CALCULATED STRESSES(average of all tendons) :

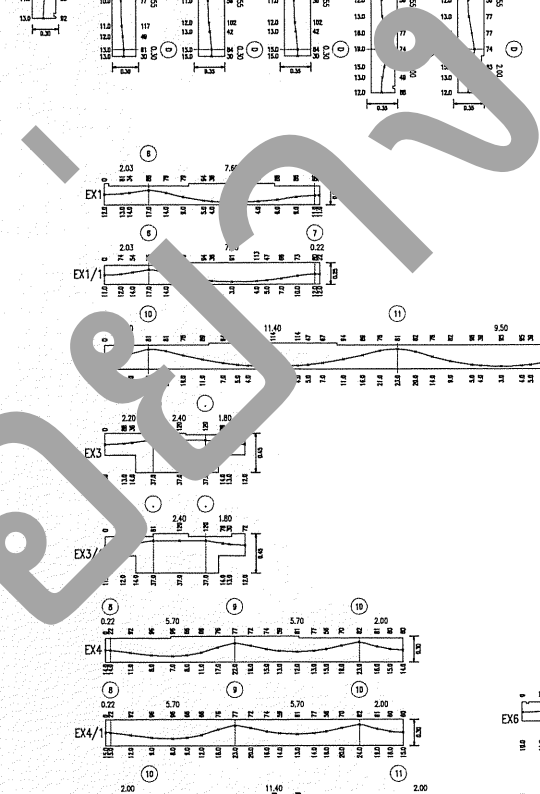
SPAN	LENGTH m	P	<TENDON HEIGHT(cm)>			Horizontal ratios			<STRESS(T/cm ²)-->		
			start	center	right	X1/L	X2/L	X3/L	start	center	right
-1-----2-----3-----4-----5-----6-----7-----8-----9-----10-----11-----12----											
CANL	3.90	2	12.0		18.7						10.95
1	7.60	2	18.7	6.2	18.7	.0	.5	.00	11.68	12.33	11.95
2	7.60	1	18.7	4.2	18.7	.0	.50	.10	11.97	11.15	10.51
3	7.60	1	18.7	4.2	12.5	.0	.50	.10	10.83	10.20	9.77

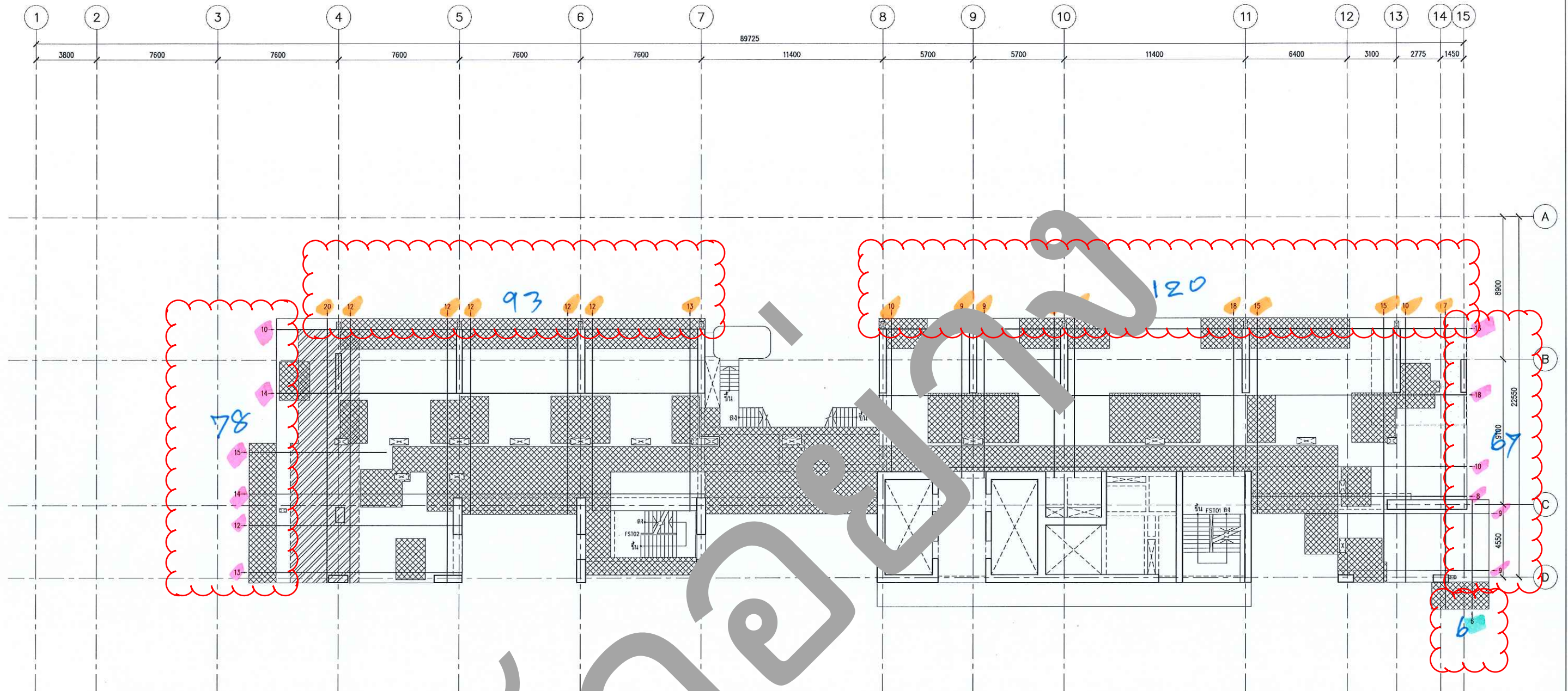
Note: P= tendon profile (refer to 1 and of data block 9)
Stresses at each location are the average of strands after anchor set,
and after long-term losses

16.8 TENDON SELECTION AND DATA:

TYPE	OFF	FORCE	<----- TENDON TENTS ----->			ELONGATION		Stress ratios	
			CAN<----->	SP A	S ----->CAN	LEFT	RIGHT	Anch.	Max.
-1-----2-----3-----4-----5-----6-----7-----8----									
A	20	10.95	<=====			15.3	.0	.66	.69
B	8	10.36	<====			2.1	.0	.56	.60
C	4	11.63	=====			.0	4.6	.62	.69

Note: Force is the average value per strand (T)
Stress ratios are at anchorage (7) and maximum along tendon (8)

[illegible]



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